

Getting the Best out of Long Scale DMM's in Metrology Application

Introduction

Long-scale multifunction DMMs now have the accuracy, resolution and stability to be used in a wide range of metrology applications. This application note describes how one such DMM can be used as an alternative to traditional equipment such as Null Detectors, Kelvin-Varley dividers, and Resistance Bridges. Practical examples are

provided, together with information on the precautions that need to be taken to ensure optimum performance, and the relative ease of use compared with traditional methods.

DMM Technology

For the purposes of this application note, a long scale DMM is defined as having an available resolution of up to $8\frac{1}{2}$ digits, this corresponds to a scale length or maximum count of $\pm 1.999\ 999\ 99$. Such resolutions are achieved by the use of multi-slope, multi-cycle analogue to digital converters (ADCs), which are the result of a long and continuous development of a basic and well known charge-balance integrating analogue to digital converter (ADC). A modern DMM¹ can achieve stabilities of better than 2 ppm per year, linearity of 1 part in 20 million, noise levels of less than 50nV, input bias current of $<10\text{pA}$ and an input resistance of $>10^{10}\Omega$ (for an input up to $\pm 20\text{V}$). This kind of performance makes them eminently suitable for metrology applications.

Practical DC Applications

Typical metrology applications include: comparing voltage standards, voltage ratio measurements and resistance transfers. For voltage standards, the comparison will typically be of two or more voltages at nominally the same level e.g. comparing two or more standards with a microvoltmeter. Provided that the meter is sensitive enough and the difference between the reference is less than $10\ \mu\text{V}$, this simple detector can give very good results and be able to resolve differences as small as $200\ \text{nV}$ ($0.2\ \text{ppm}$ of 1V). However, if the standards have a large voltage spread, or if standards at different temperatures are compared, the differences could be as large as a millivolt. A typical microvoltmeter under these conditions would only resolve $20\ \mu\text{V}$ on its 1mV range, due to the fundamental limitations of scale length and resolution. A long-scale DMM on its 100mV range can resolve 10nV . Subject to noise limitations, it could measure two cells that were well over 100mV apart and still resolve 10nV . Electronic, Zener-based references are now widely



used and often have outputs at the 10V, 1V and 1.018V levels. Comparison between the different voltage outputs requires knowledge of the voltage ratio. Traditionally, high-precision voltage dividers would be used for this task, a known voltage at the 10V level would be divided by a known ratio through the (calibrated) divider and compared at the 1V or 1.018V level using a microvoltmeter. The divider would have to be known for all the required ratios and would be adjusted to null the microvoltmeter. A linear, long-scale DMM can replace these instruments and simplify the measurement. Figure 1 shows the basic arrangement for comparing two standards at the 10V level - the connections would be very similar for 1V or 1.018V.

Note that the arrangement is very similar to that described for DC standards except that now, the DMM (rather than a microvoltmeter) can handle large differences between the two devices without sacrificing resolution. There are no significant problems with this measurement provided that the DMM's isolation to ground does

not load the output of either voltage reference and that a preliminary zero operation is performed to remove any residual offsets in the DMM and its connecting leads. The configuration shown is effectively a potentiometric or differential measurement. The DMM is configured to measure the difference between the two voltage references.

Ratio Mode and Rear Inputs

The 1281 DMM¹ has 3 input channels, two of which (Channels A and B) may be automatically switched to perform a ratio measurement. In ratio mode, the DMM displays the ratio of the inputs in the form A-B, or A/B(%), or (A-B)/B(%). The most commonly used of these ratios is A/B(%). In this mode with, for example, 10V connected to channel B (reference) and 1V connected to channel A, the display would show +10.000 000%. This is the ratio of the unknown 1V to the known 10V reference. Note that the DMM is measuring the whole voltage for each channel and is configured to a single (10V) range. The only error

contributions to this measurement are the uncertainty of the 10V reference standard, the noise and differential linearity of the DMM and the noise of the UUT 1V standard. Typical noise of the DMM is <50nV and differential linearity in 8½ digit mode is better than 0.1 ppm of FS over a 10:1 ratio. These figures are similar to that which might be obtained by a skilled metrologist with a freshly calibrated voltage divider and microvoltmeter. The DMM can make this measurement continuously and its linearity does not change significantly with time, so set up costs are lower and the measurement takes less time. Figure 2 shows how the DMM can be used to measure the whole voltage of each reference by using identical multiple input channels in the ratio mode.

Confirmation of the DMM's linearity beyond the 0.1 ppm level is difficult under normal circumstances. However, several instruments of varying age have now been evaluated by national laboratories against 10V Josephson arrays. In this measurement, the Josephson system can be made to generate

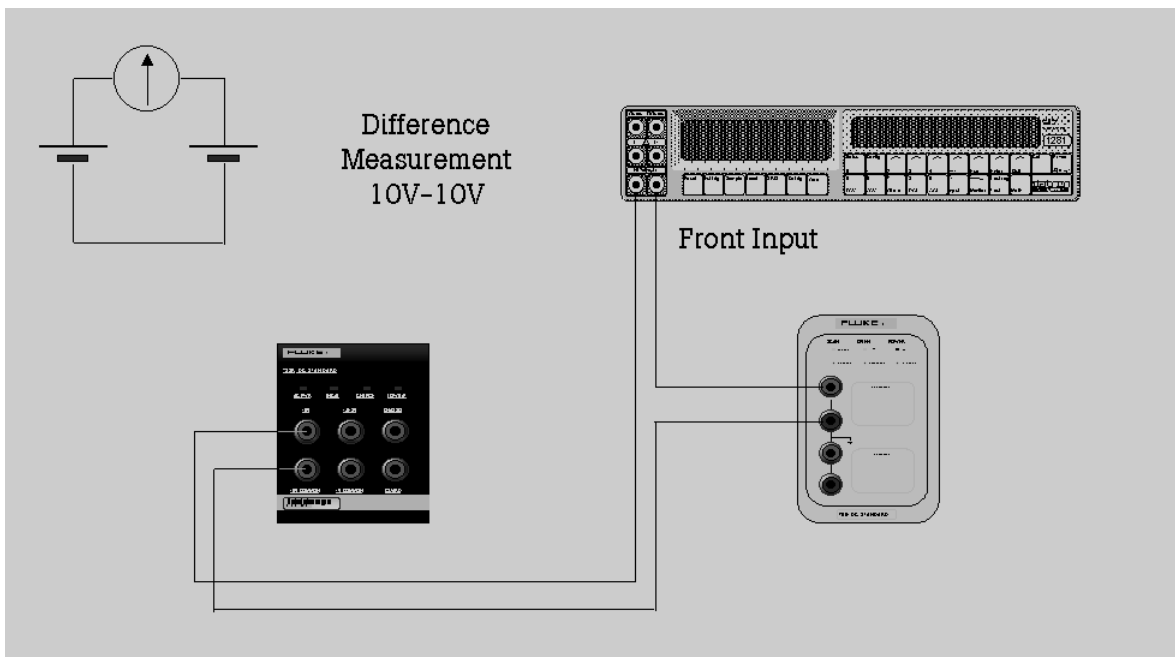


Figure 1 Voltage Difference Measurement

a series of voltages between 1V and 10V with uncertainties at least an order of magnitude better than the DMM's linearity.

Resistance Applications

Another very useful application of the long-scale DMM is in resistance measurements. An 8½ digit DMM of the type described above has virtually the same linearity on its resistance function as for DC voltage, except, in this case, there are no resistance standards accurate enough to be able to prove resistance linearity in a conventional sense. One of the problems of trying to measure resistance linearity directly is the uncertainty of the individual resistor values². For example, measuring linearity on the 10kΩ range of an 8½ digit DMM with a maximum indication of 19.000 000 0 kΩ would require several different resistance standards. Assuming that measurements were to be made at a minimum of five evenly spaced points throughout the range e.g. at zero, 5kΩ, 10kΩ, 15kΩ, and 19.9kΩ, the difficulties in finding suitable standards soon become obvious. Typically, resistance standards will be available at the normal decade values of 10Ω (25Ω may be available), 100Ω, 1kΩ, 10kΩ, etc. and so do not provide

even coverage throughout the range. When one considers that some DMMs have resistance linearity specifications of better than 0.3 ppm, and that individual resistance standards may have uncertainties of 1 ppm or more, test methods using separate resistors or decade boxes will be inadequate. For this reason, resistance linearity is not usually measured during routine calibrations of long-scale DMM's. However, linearity can be verified in the following way. Figure 3 shows the circuit configuration for resistance measurement used in a high accuracy DMM.

The resistance option is primarily a range of selectable constant currents. A constant current generator forces a current Ix to flow through the test resistor Rx. A true constant current source will generate a current independently of the voltage developed across its terminals, in this case designated I+ and I-. It therefore follows that if a known resistance is applied to the DMM and the display value noted, the insertion of an additional resistance in series with the I+ lead should not significantly affect the DMM's reading. This will confirm that the current source can deliver the same current through a range of resistance values. If it can also be confirmed

that the voltage range used for the resistance measurement is also linear, there is then a technically sound way of confirming good resistance linearity without the need for a resistance linearity standard. Note that the series resistance does not need to be a precision resistor - it could be a low-noise potentiometer.

True Ohms

It is natural that four wire sensing techniques will be used for the measurement of lower value resistors of <10kΩ, but what about the effects of voltage offsets? Offsets in resistance measurements have two basic forms or origins. The first of these is the static offset and is caused by junctions of dissimilar metals in the voltage measuring circuit. Typical sources might be within the resistor itself, or connecting leads and terminals. There will also be voltage offsets in the DMM. A simple zero operation (a mathematical subtraction) before the measurement commences will remove these offsets. The second type of offset is dynamic and has a thermal time constant. It is primarily caused by the direct heating of the resistor by the energizing current, but where large currents are involved, can also give rise to thermo-electric effects

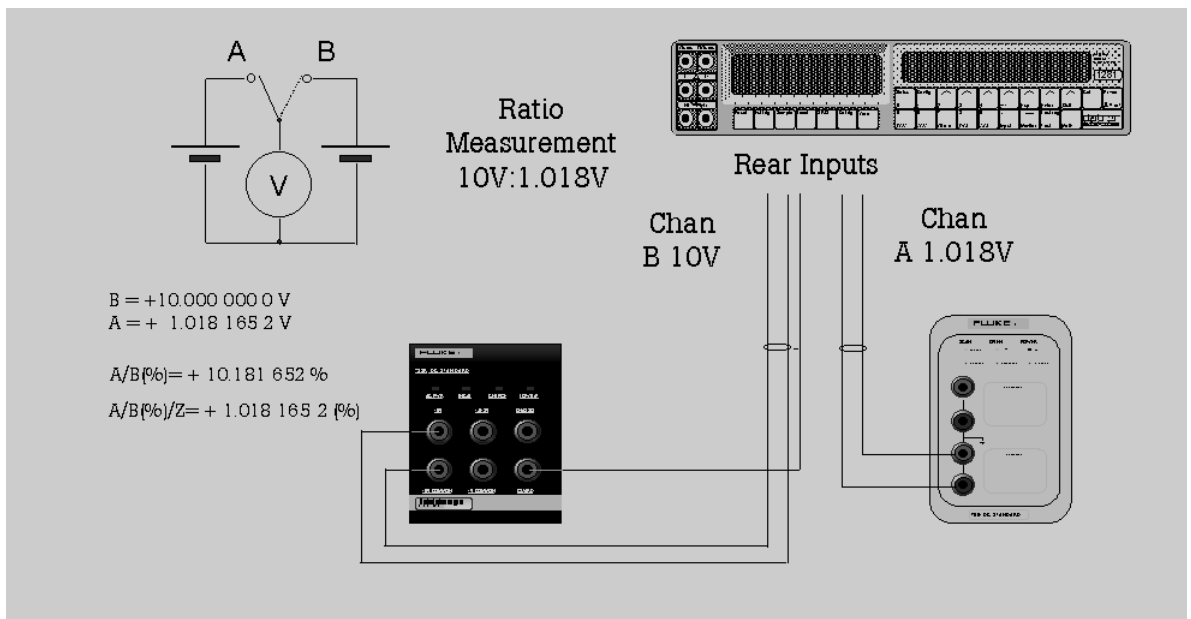


Figure 2 Voltage Ratio Measurement

(Peltier and Seebeck) in external connections too. These dynamic thermal offsets only occur when the current is flowing but because of their long thermal time-constant, can be measured.

Traditional resistance bridge measurements use a specific process to isolate resistance from other unwanted parasitics i.e. voltage offsets. A typical arrangement would be to place the known and unknown resistors in series and pass a

current through them. A voltage ratio measurement would then be made of the voltages developed across the potential terminals of each resistor. The current supply would then be reversed and the measurement repeated. The current reversal will remove the effects of the voltage offsets because in one polarity they would add to the measured voltage and in the reverse polarity would subtract from it. The average voltage

ratio from the forward and reverse currents will remove the offsets. True Ohms is also very effective (although the current is not reversed); a sequence of measurements is made alternately switching the current through the unknown resistor or via a current bypass (to improve settling). The voltage measured across the resistor with no current flowing is subtracted from that developed across the resistor with the

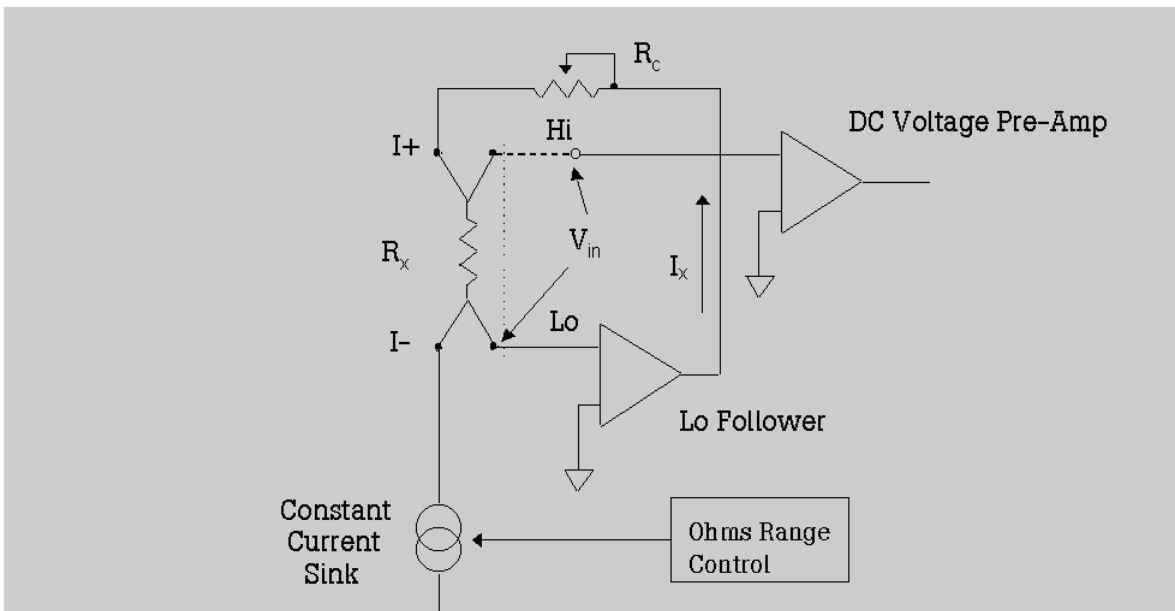


Figure 3 DMM Ohms Converter

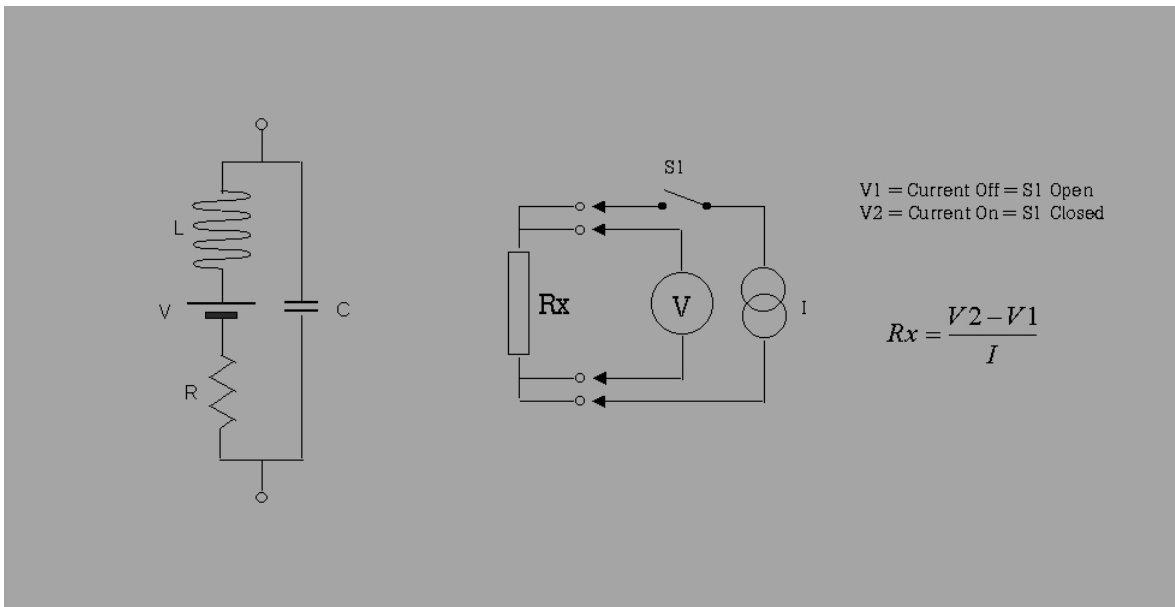


Figure 4a Resistor Parasitics

Figure 4b True Ohms Principle

current flowing through it. Although a very simple process, it is very effective and can cope easily with changing thermal offsets. Figure 4 shows the true ohms principal. The on-off cycle timing of the current through the resistor is carefully chosen to ensure maximum rejection of dynamic offsets. True Ohms would normally only be used for the measurement of resistors up to 1kΩ (although it is available up to 100kΩ). There is little effect from thermal emfs above this value and the reactive time constant of the resistor may introduce settling errors. A resistor can be modeled as shown in Figure 4a with a series voltage source (thermal offset), series inductance and parallel capacitance. For values up to 100Ω, neither the inductance or capacitance will have any effect, but at 10kΩ and above (where offsets are not usually a problem), depending on the resistor construction, the voltage may never settle in a true ohms measurement.

Ohms Guard

Another consideration is the

effect of parallel leakages in the measurement circuit. Such leakages will divert some current away from the resistor being measured and cause an error in the measurement. A DMM's Ohms Guard can effectively remove the effects of leakage provided that a suitable connection for the guard is available. Figure 5 shows the 1281 DMM's Ohms guard in use.

The Lo Follower will maintain Lo and Analog Common (OV) at the same potential by forcing more current through Rx and Ra until Lo is at OV (Ib=0). The calibrated current Ix will then be flowing through Rx. Note that where the connection lead insulation is suspect, running I+ and Hi in one shield and I- and Lo in another, while connecting both shields to Ohms guard, will remove any leakage between Hi/I+ and Lo/I- because the leakage is "seen" as a parallel resistance path with a convenient tapping (the cable screens) for Ohms guard. Provided the leakage path is less than 250Ω, not only will the leakage current be sourced from the Lo follower (as Ia), but any lead capacitance charge

current will also be driven resulting in reduced settling times for high value resistors.

Resistance Transfers and Ratio

True Ohms and Ohms guard are both available from the DMM front and rear inputs; this means that lead leakage can be eliminated from high resistance measurements and voltage offsets eliminated from low resistance measurements. When combined with ratio switching, very high accuracy automated resistance transfers can be performed for both 1:1 and 10:1 ratios. In either case, the DMM will be configured for the appropriate resolution (4½ to 8½ digits), ADC speed, Ohms source current, analog/digital filter and ratio mode for the particular resistor values concerned. The range selection will be chosen to accommodate the higher of the two resistor values. For example, a 10kΩ to 1kΩ ratio will use the DMM's 10kΩ range - the DMM's excellent linearity will ensure the maximum transfer accuracy between the two values. Figure 6 shows the DMM configured via the rear inputs to compare

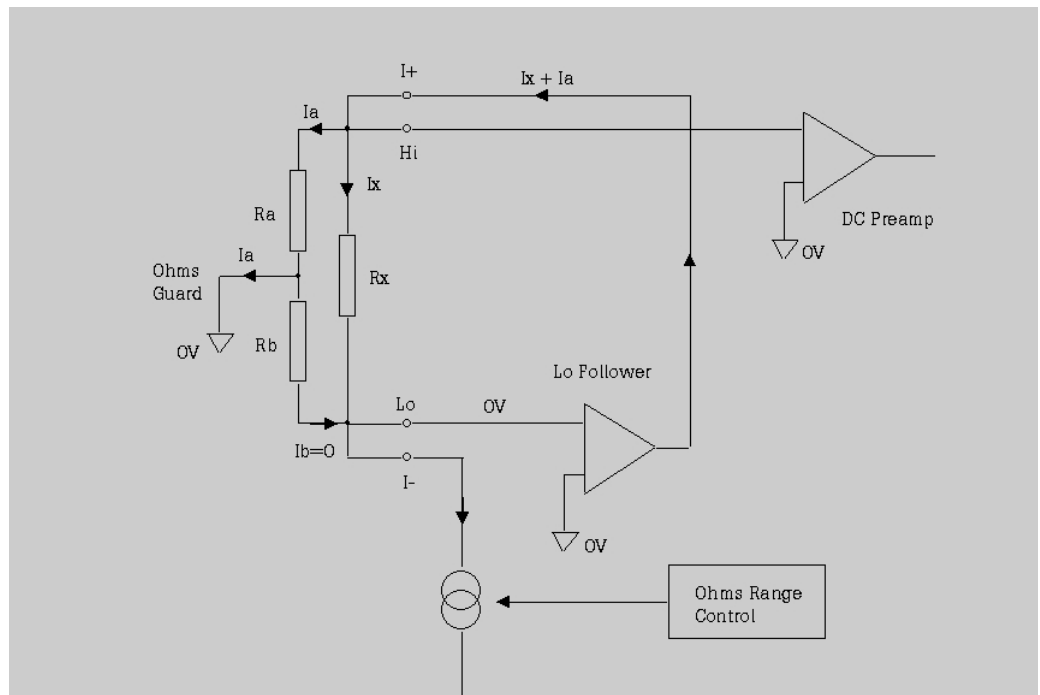


Figure 5 Ohms Guard Operation

two resistance standards using resistance ratio.

Where the value of the resistors to be measured is low e.g. 100Ω or less, a voltage ratio method can also be used. In this mode an external current source provides the test current which is passed through the series connected resistors. The DMM is used in its voltage ratio mode. The DMM's internal current source provides a maximum current of 10mA . Using the voltage ratio mode as shown in Figure 7, a 100mA , 1A or 10A source could be used. This method allows the resistance ratio range to be extended to include values below 1Ω , e.g. $100\text{m}\Omega$, $10\text{m}\Omega$ or even $1\text{m}\Omega$. As mentioned earlier, thermal offsets will be significant for low value resistors - particularly where high currents

are involved, therefore it will normally be necessary to reverse the current and take the average of the two voltage ratio measurements.

Decade Box Calibration

For the calibration of decade resistor boxes, the most convenient method is to use the DMM's accuracy for a direct measurement i.e. not in ratio mode. This is because of the number of measurements required and the reduced accuracy needed for most decade boxes. Most decade boxes are two terminal with a significant zero resistance. True Ohms is very effective for this kind of measurement because it will remove voltage offsets but not be affected by resistance offsets - although the DMM's input zero function can be used

to suppress these also. Figure 8 shows a decade box connected to the DMM on channel A. Channel B would not normally be used, but for the utmost accuracy (a waste of time on most decade boxes!), a transfer could easily be made to a resistance standard connected to channel B. Note that the front input could also be used for either resistor.

A two-wire, six-dial decade box of nominally $10\text{k}\Omega$ would require four ranges of the DMM to be used. The DMM would be used in the True Ohms mode with the ranges and resolution set as shown in Table 1. First, a four-wire zero would be made by connecting I+ and Hi to Lo and I- at the decade box Lo terminal. The input zero is then used to remove any residual resistance offset. The DMM Hi

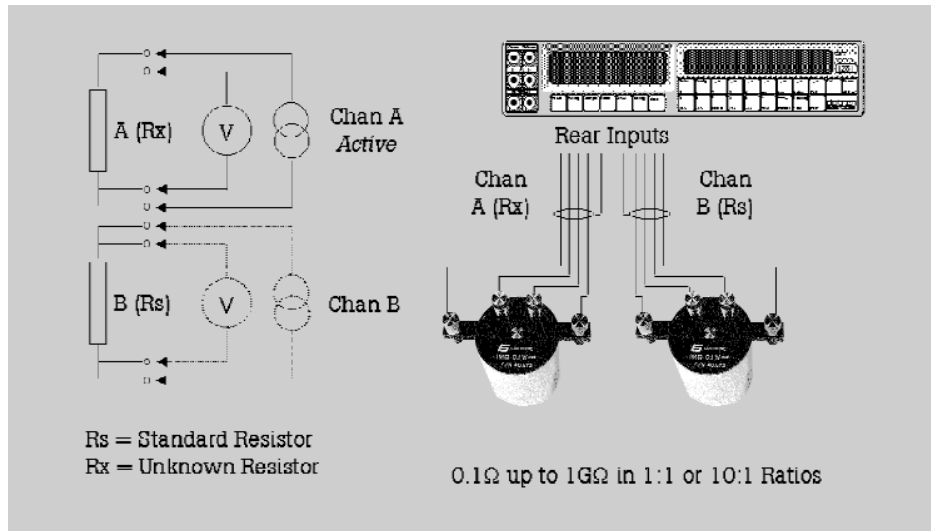


Figure 6 Resistance Ratio

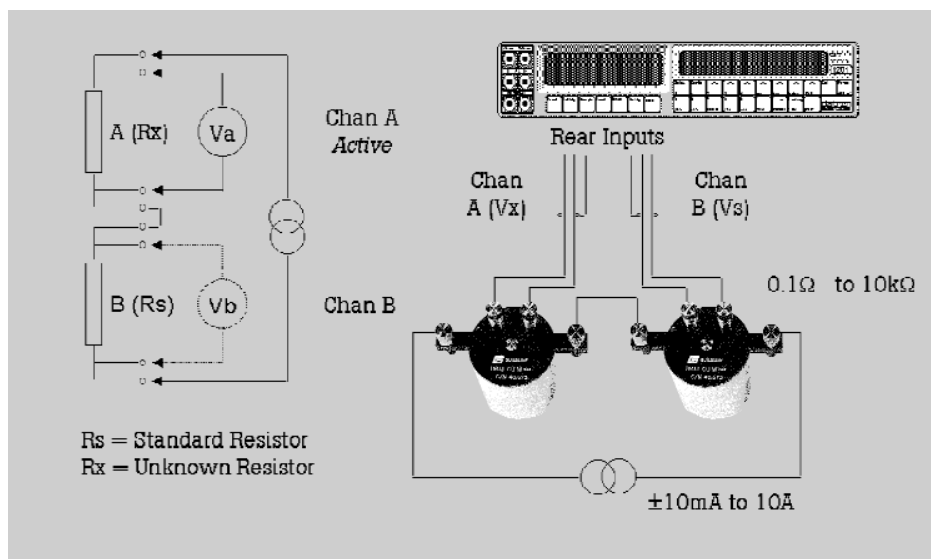


Figure 7 Voltage Ratio (Resistance)

and I+ wires would then be moved to the resistor Hi with all decades set to zero. The DMM will indicate the true zero error of the decade box. After recording the zero value, the resistance offset will be removed by the input zero function and each decade measured in turn at each dial setting up to a maximum of 11.1111kΩ. Note that from the resolution table, the relative accuracy of this measurement is very high, and because the DMM resolution is adjusted for each decade, it will also be very fast.

Conclusions

The long-scale DMM has

become a very valuable and versatile instrument for high-accuracy metrology applications and is widely used in commercial, military and national standards laboratories. It is a viable and cost-effective alternative to traditional methods and can greatly facilitate automation. This application note has only discussed applications of the DMM, there are other areas of measurement where such a DMM is invaluable, such as current measurements where the DMM is used to measure the voltage developed across a known resistive current shunt. There are also several applications that may be the subject of a future application note.

Dial #	Step Value	Decade Maximum	DMM Range	DMM Digits	Measurement Resolution	
					% of Step	ppm of 10kW
1	1kΩ	10 kΩ	10 kΩ	7½ d	0.0001%	0.1 ppm
2	100Ω	1kΩ	1kΩ	6½ d	0.001%	0.1 ppm
3	10Ω	100Ω	100Ω	5½ d	0.01%	0.1 ppm
4	1Ω	10Ω	10Ω	5½ d	0.01%	0.01 ppm
5	0.1Ω	1Ω	10Ω	4½ d	1%	0.1 ppm
6	0.01Ω	0.1Ω	10Ω	4½ d	10%	0.1 ppm

Table 1 Decade Box and DMM Resolution

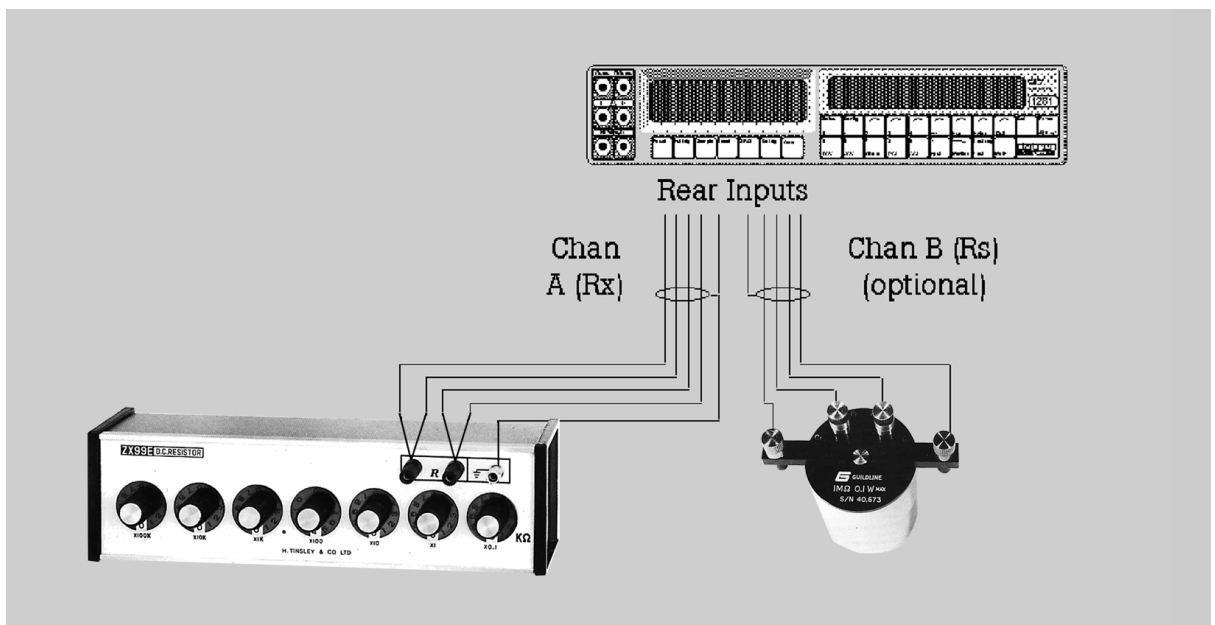


Figure 8 Decade Box Calibration

References

- [1] Model 1281 Selfcal Digital Multimeter User 's Handbook, Fluke Precision Measurement Ltd.,UK.
- [2] "A Generic DMM Test and Calibration Strategy ". Author:Peter Crisp, Fluke Precision Measurement, UK.
- [3] "A Guide to measuring resistance and impedance below 1MHZ" Institute of Measurement and Control.

Acknowledgements

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